

Characteristics of soluble mixtures

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Outline

- **Geo-soluble mixtures**

- Introduction

- Testing

- Numerical Modeling

- Summary

Introduction

- Soil naturally contains grains of different mineral → dissolved
- Dissolution → change microstructure:
 - ↑ local void + permeability
 - influence the safety

St. Francis Dam Failure



The small strain stiffness of soluble mixtures modeled by sand-salt mixtures with various salt volume fractions.

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Materials

Jumunjin Sand



Salt



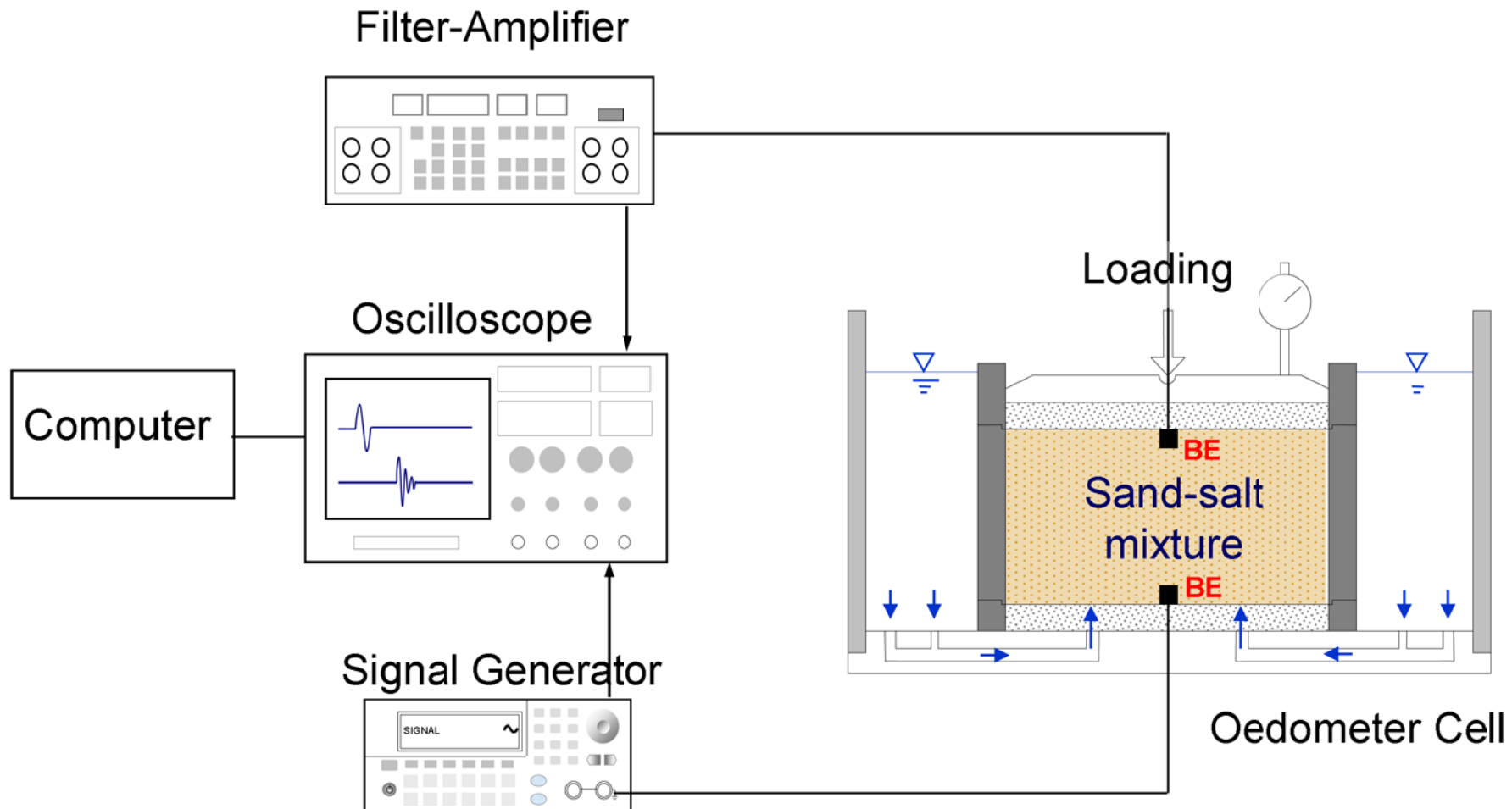
500um

	G_s	D_{50} (mm)	S	R
Sand	2.62	0.36	0.65	0.7
Salt	2.16	0.25	0.73	0.27

- Mean grain size of sand particles ≈ 1.5 times larger than that of salt particle

Experimental setup

- The effect of dissolution – micro to macro mechanical behavior of mixtures – implementing S-wave measurement.
- BE – top cap & bottom plate

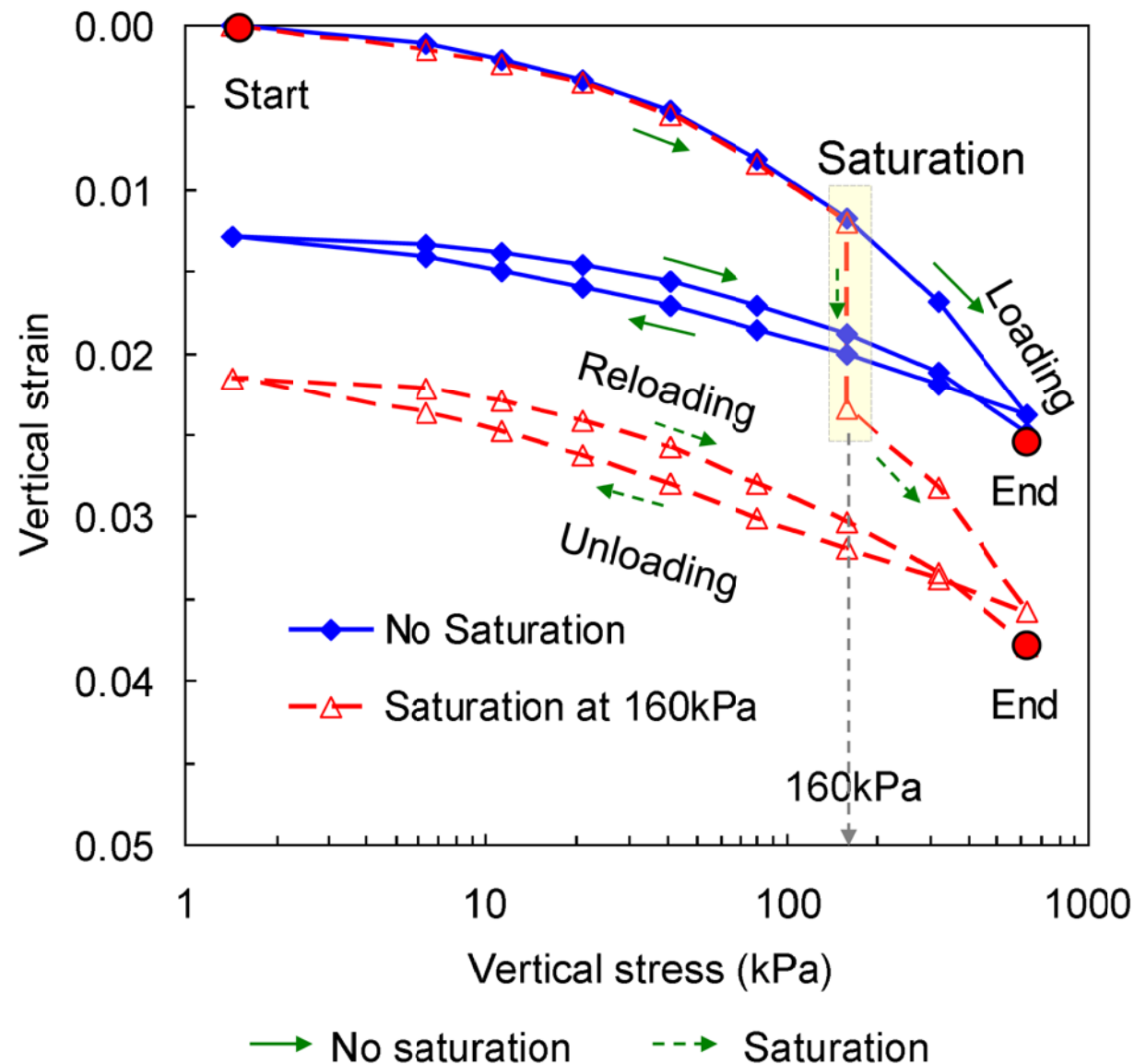


Test procedure

- Soluble mixtures – prepared different salt content- volume fraction
 - Salt fraction: $sf = V_{\text{salt}}/V_{\text{sand}} (\%)$
 - Specimens with $sf = 0, 2, 5, 7, \& 10 \%$
 - 5 layers, tamping (same energy)
- 3 stages: loading – unloading – reloading with time interval:
 - Loading – unloading stage: 30 minutes
 - Saturation stage: 1000 minutes
- Stress for saturation: used NaCl 0.01 - different confining stresses
- Shear wave measurement: at the end of loading step

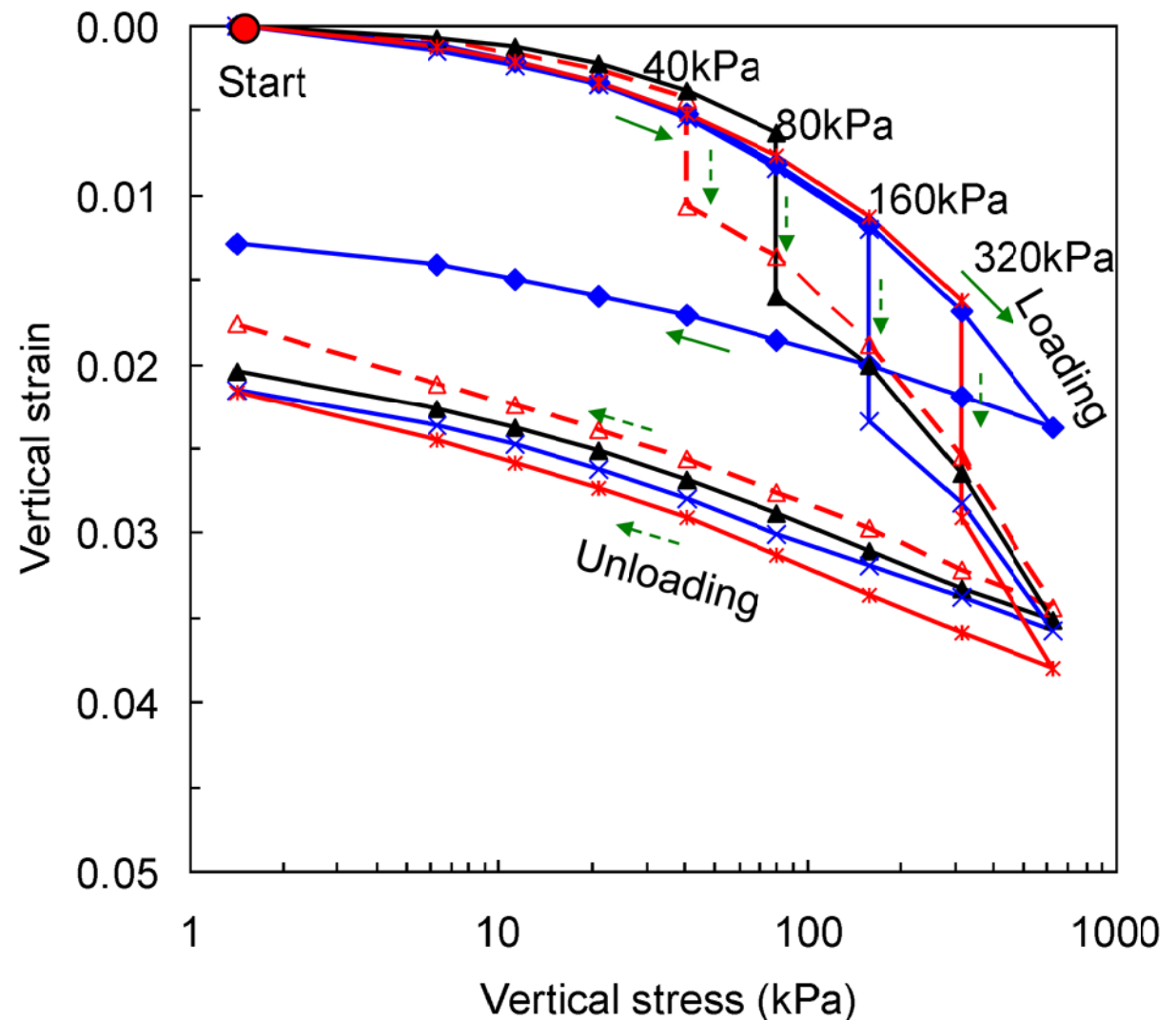
Vertical strain - Saturation

- Vertical strain of 2 mixtures with 10% initial salt fraction
- 1: no dissolved
- 2: dissolved at 160kPa
- Before saturation:
 - identical behavior
- After saturation:
 - $\epsilon_v \uparrow$



Vertical strain – Different vertical stresses

- Vertical strain: mixtures
10% initial salt fraction –
saturated – different
stresses.
- Dissolved at various σ_v^s
= 40 ~ 320kPa
- As the planned stress
increase, the total
vertical strain increase:
 $\sigma_v \uparrow \quad \varepsilon_v \uparrow$

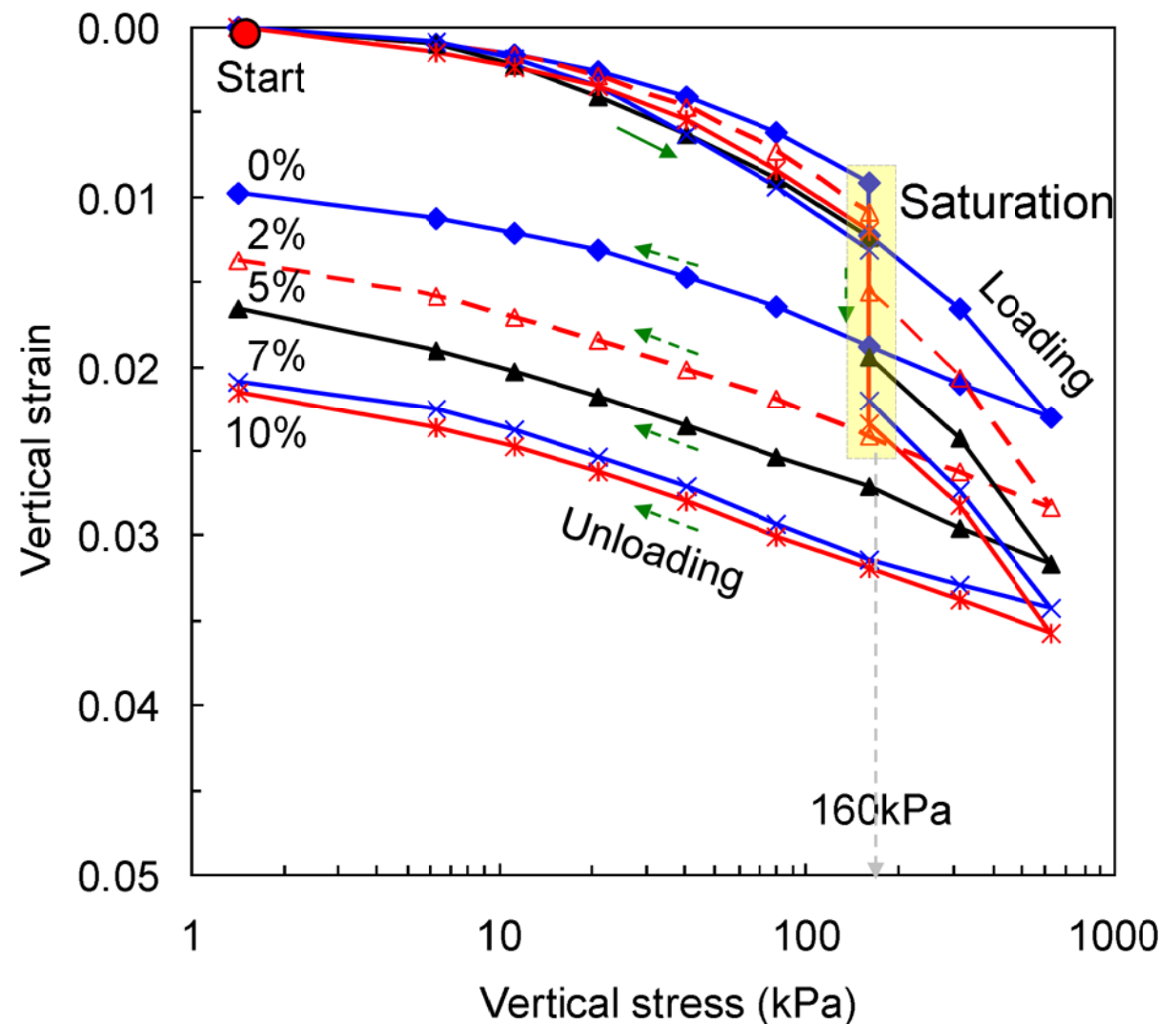


Vertical strain – Different salt fractions

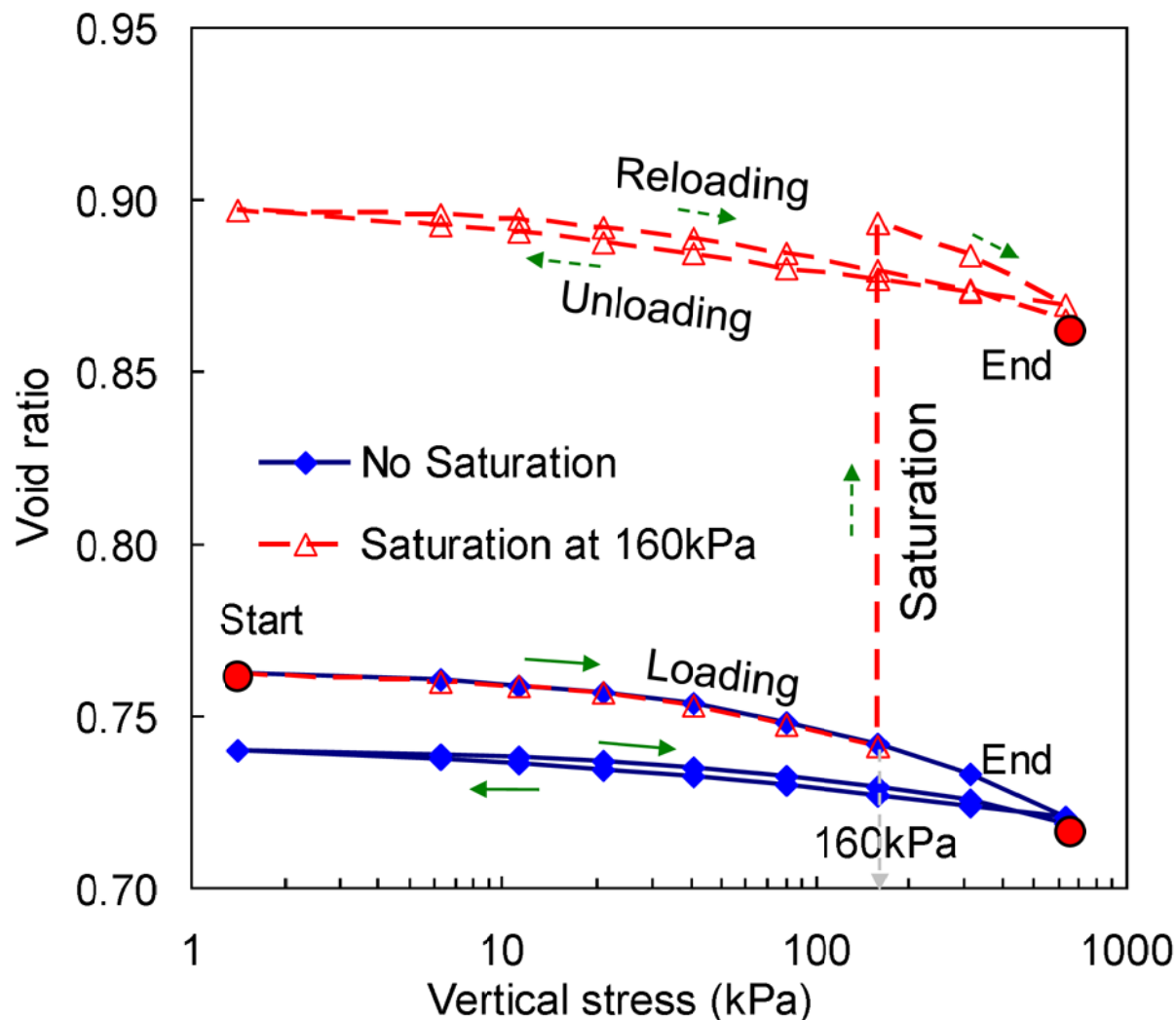
- Specimens: different initial sf: 0~10%
- Saturated at $\sigma_v = 160\text{kPa}$
- sf \uparrow ϵ_v \uparrow

∴ Total volume \downarrow after dissolution

∴ Specimens seems to be getting **stiffer**

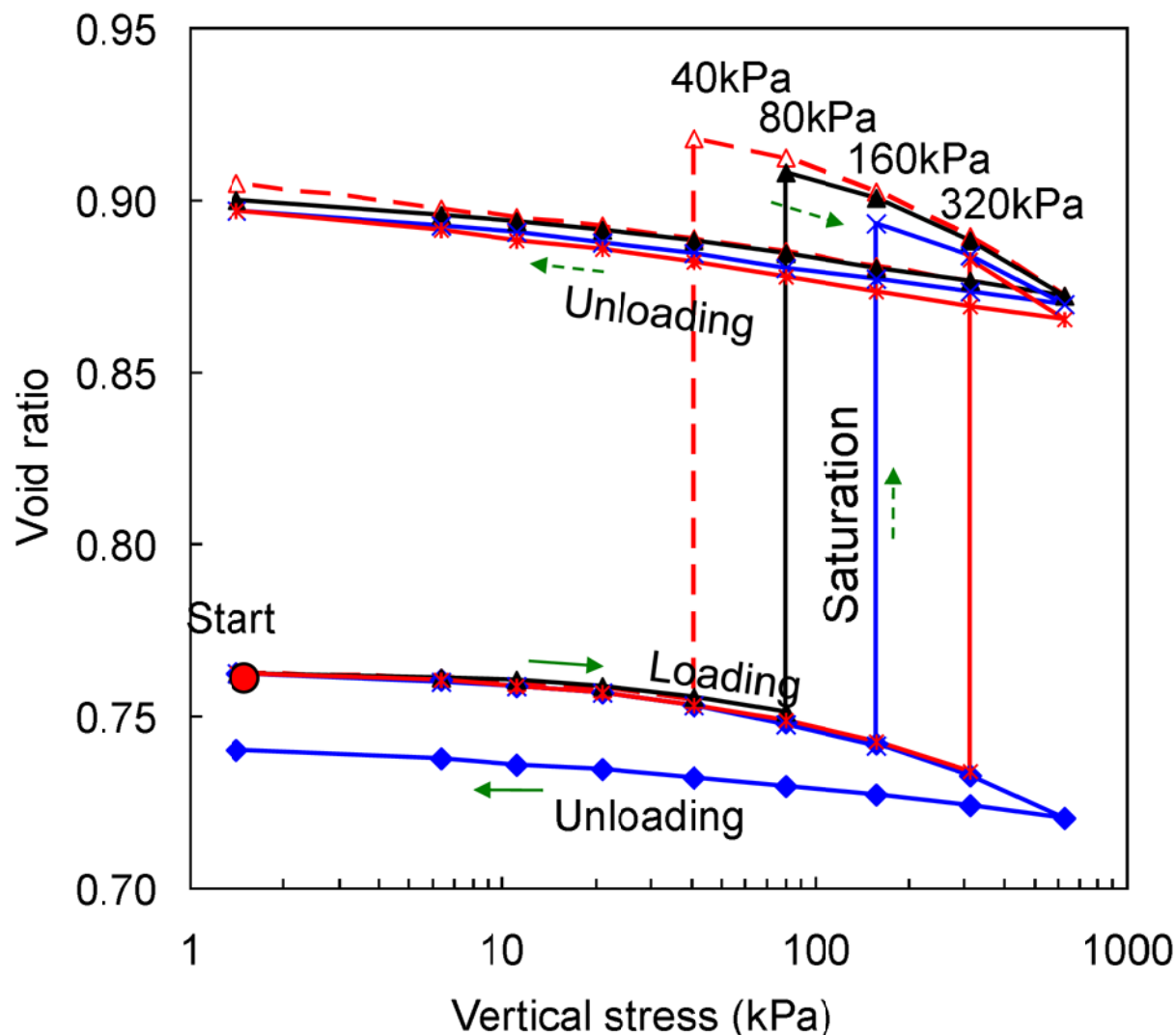


Void ratio – Saturation



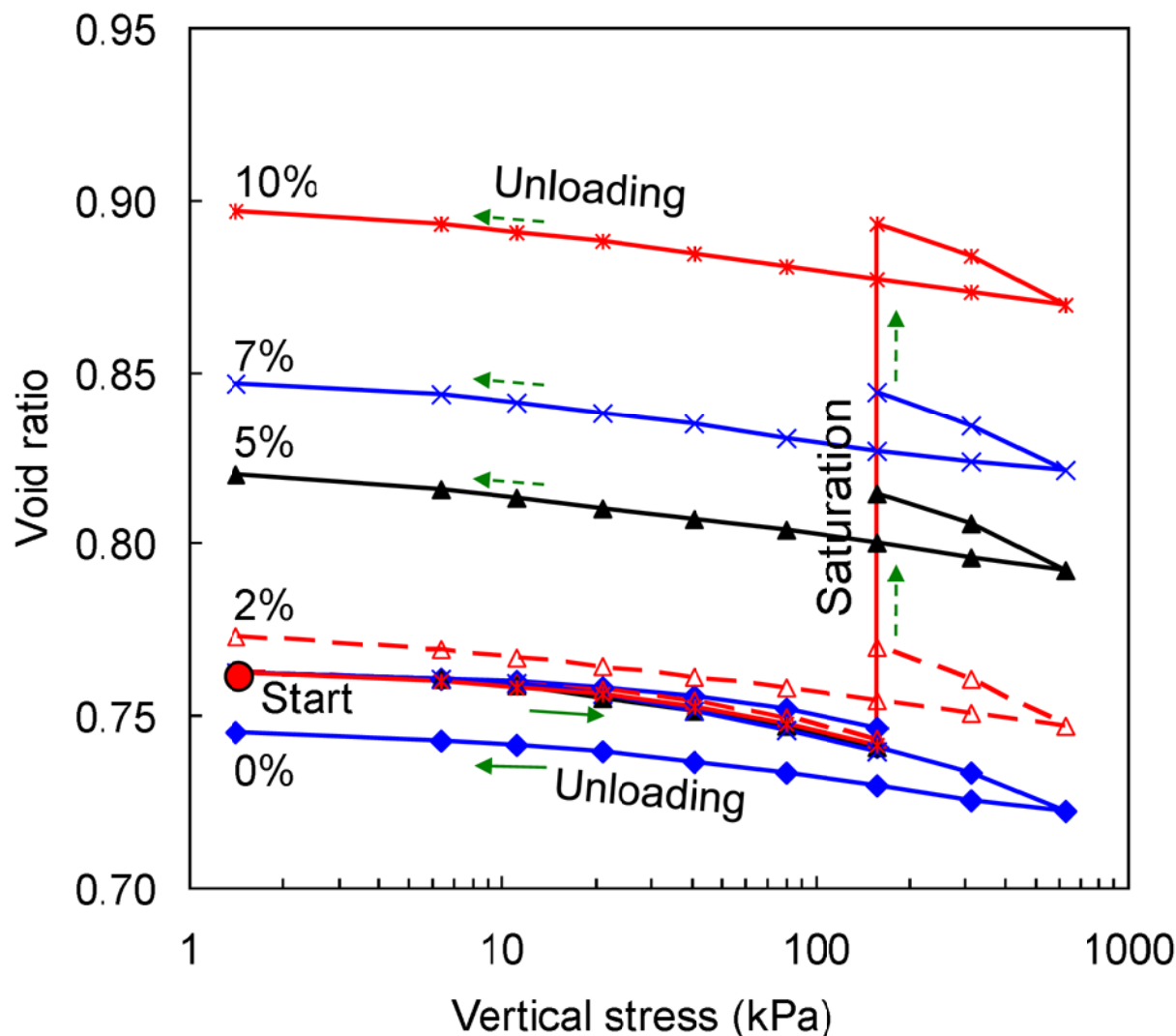
- Change of void ratio for 2 mixtures –10% sf
- 1: no dissolved
- 2: dissolved at 160kPa
- Before saturation:
 - Same behavior
- After saturation:
 - $e \uparrow \uparrow \leftarrow$ dissolution of salt particles

Void ratio – Different vertical stresses



- Change of void ratio of the mixtures - 10% sf
- Saturated at different $\sigma_v^s = 40 \sim 320 \text{ kPa}$
- Before saturation:
 - Same behavior
- At saturated stress:
 - $\sigma_v \uparrow$ e \downarrow : lower saturated stress – higher void ratio

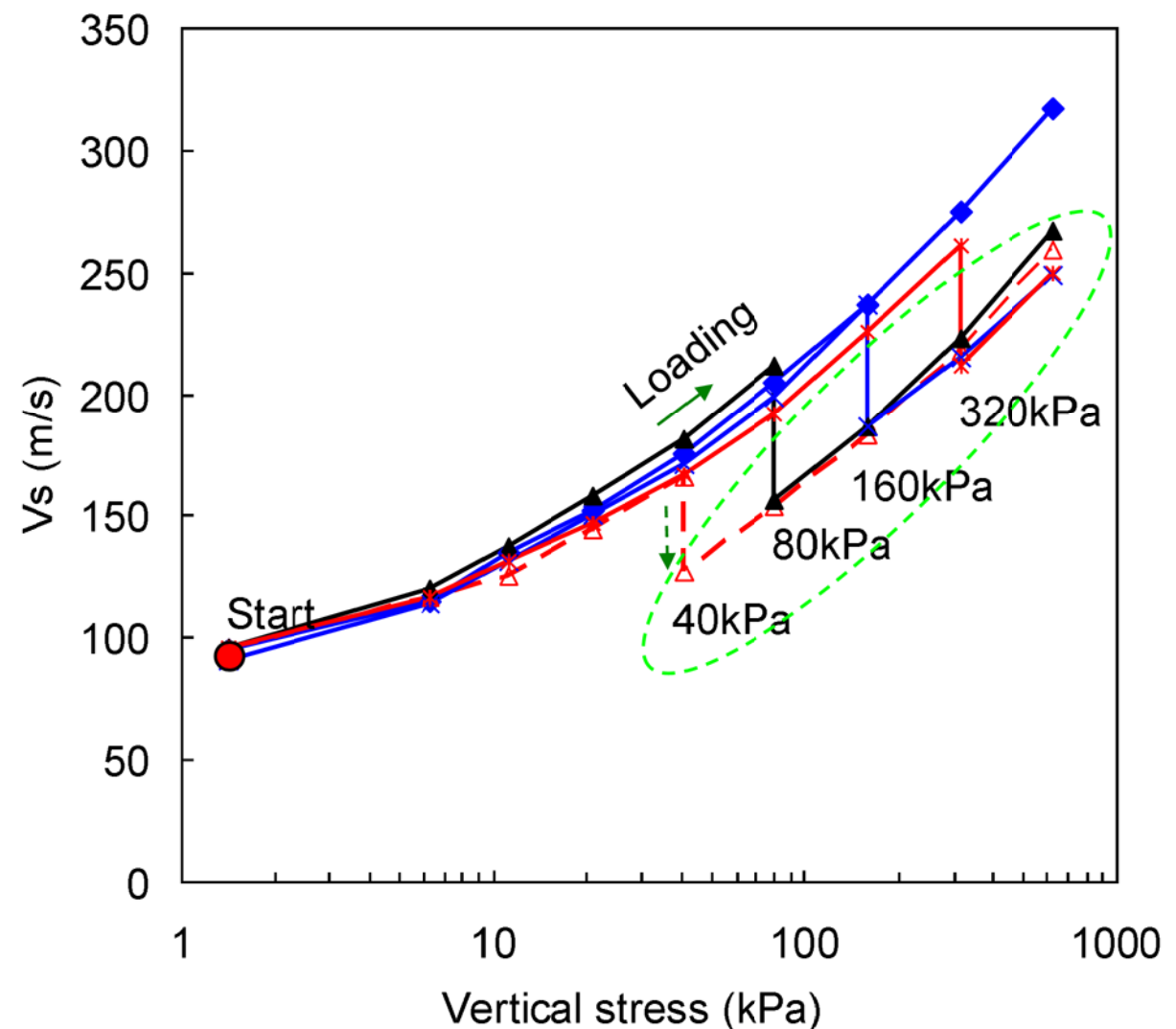
Void ratio - Different salt fractions



- Evolution of void ratio – mixtures - 0 ~ 10% sf
- Saturated: $\sigma_v^s = 160 \text{ kPa}$
- Before saturation:
 - Same behavior
- At saturated stress:
 - $\text{sf} \uparrow \text{ } e \uparrow$: higher initial sf, higher void ratio
- Specimens getting loosen due to the dissolution

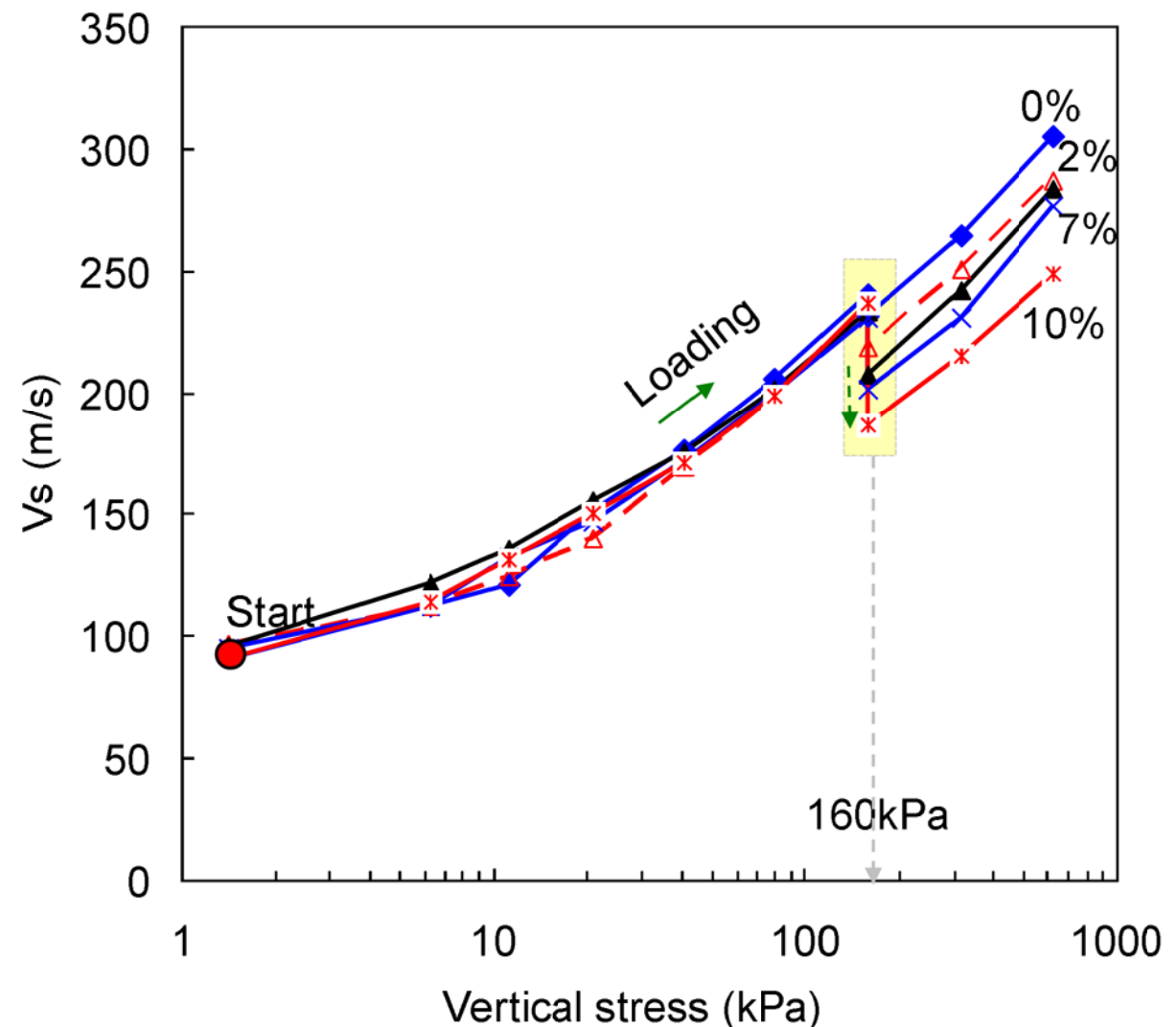
S-wave velocity - Different vertical stresses

- Shear wave velocities – specimens 10% initial sf
- Saturated at different $\sigma_v^s = 40 \sim 320\text{kPa}$
- $V_s \downarrow$ due to dissolution
- V_s after sat. collapses to 1 single line
- $V_s \downarrow$ about 26%~19% at $\sigma_v^s = 40 \sim 320\text{kPa}$



S-wave velocity – Different salt fractions

- Shear wave velocities
- specimens: 0 ~ 10%
initial sf
- Saturated at fixed
 σ_v^s : 160kPa
- Decrement of V_s -
proportional to the
initial sf



Discussions

- Shear wave velocities can be expressed in term – effective stress

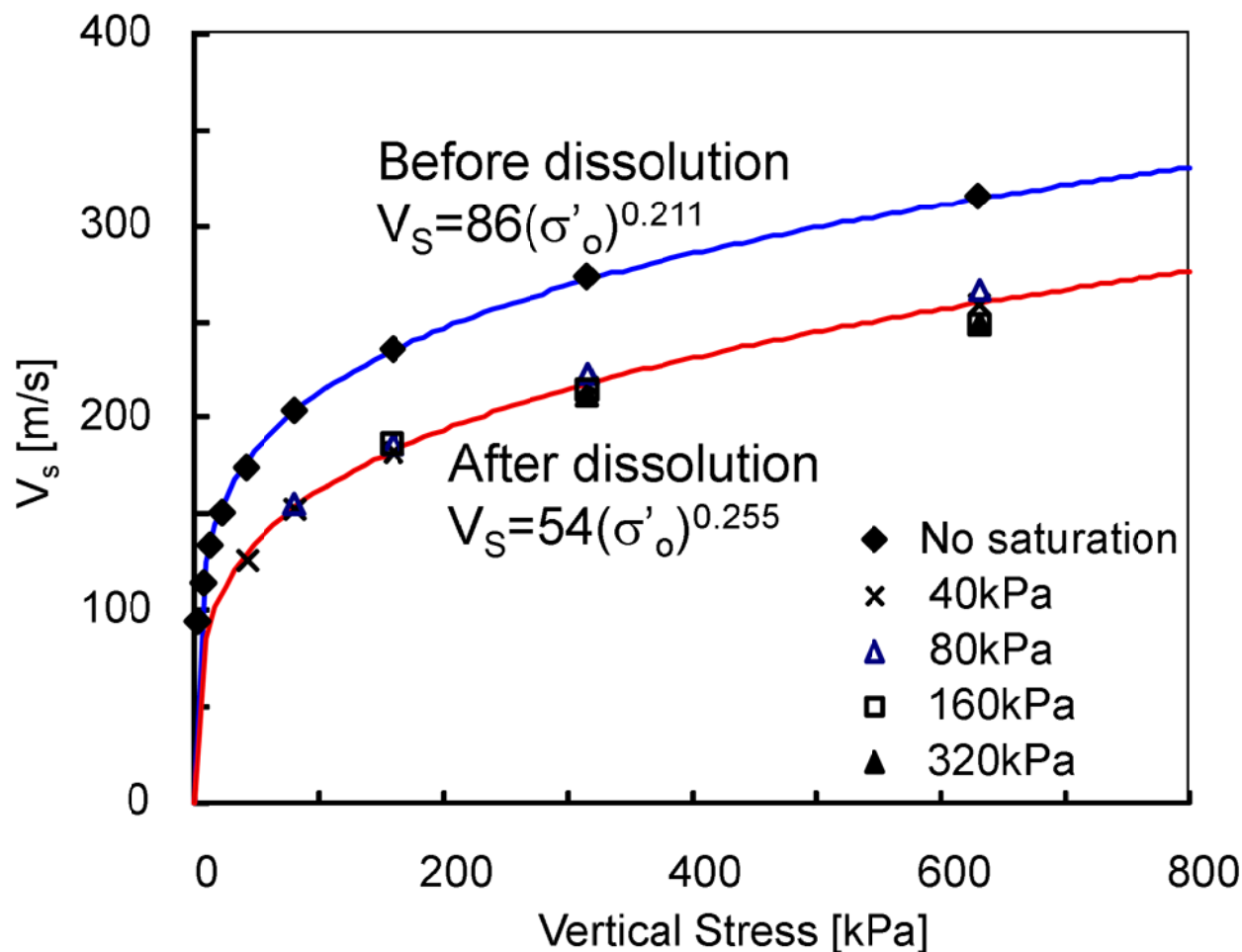
$$V_s = \alpha \left(\frac{\sigma'_0}{1kPa} \right)^\beta = \alpha \left(\frac{\sigma'_p + \sigma'_m}{2kPa} \right)^\beta = Af(e) \left(\frac{(1 + K_o) \sigma'_p}{2kPa} \right)^\beta$$

- σ'_p & σ'_m – effective stress in direction of wave propagation & of particle motion
- α , β & A : experimentally determined
- β : relates to contact behavior of media – size, structure, shape of particles
- α : represents type of packing (porosity – coordination number), the properties of grain materials & fabric changes

- $$f(e) = \frac{2.97 - e}{\sqrt{1 + e}} \quad (\text{Hardin and Drnevich, 1972})$$

Discussions

- Investigation of A & $f(e)$ → mechanical behavior of mixtures after dissolution
- Shear wave velocity vs. σ' – specimens 10% sf → collapse 1 single line



■ $e \uparrow \approx 21\%$

■ $\alpha: 86 \rightarrow 54$

■ $f(e) \downarrow - 11\%$

∴ $A \downarrow - 30\%$

∴ A-factor \downarrow implies a loss of the particle contact after dissolution.

→ $\beta \uparrow \alpha \downarrow$ - loosen specimens.

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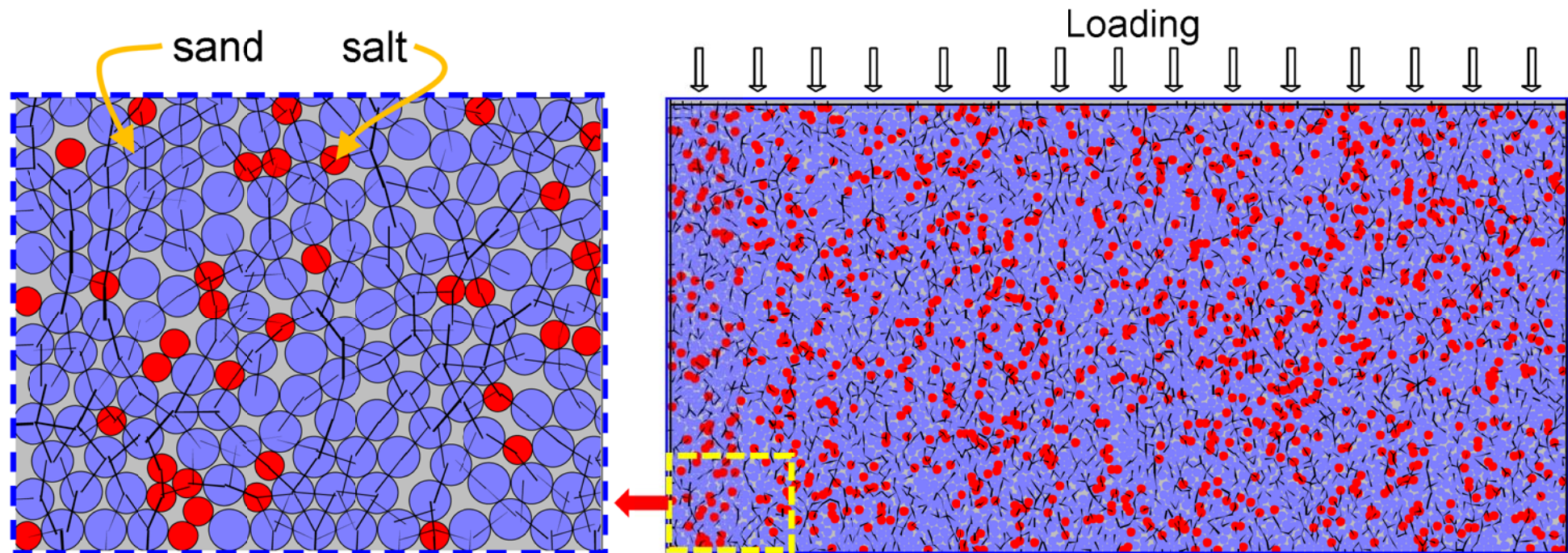
- Testing

- Numerical Modeling

- Summary

Sample Preparation

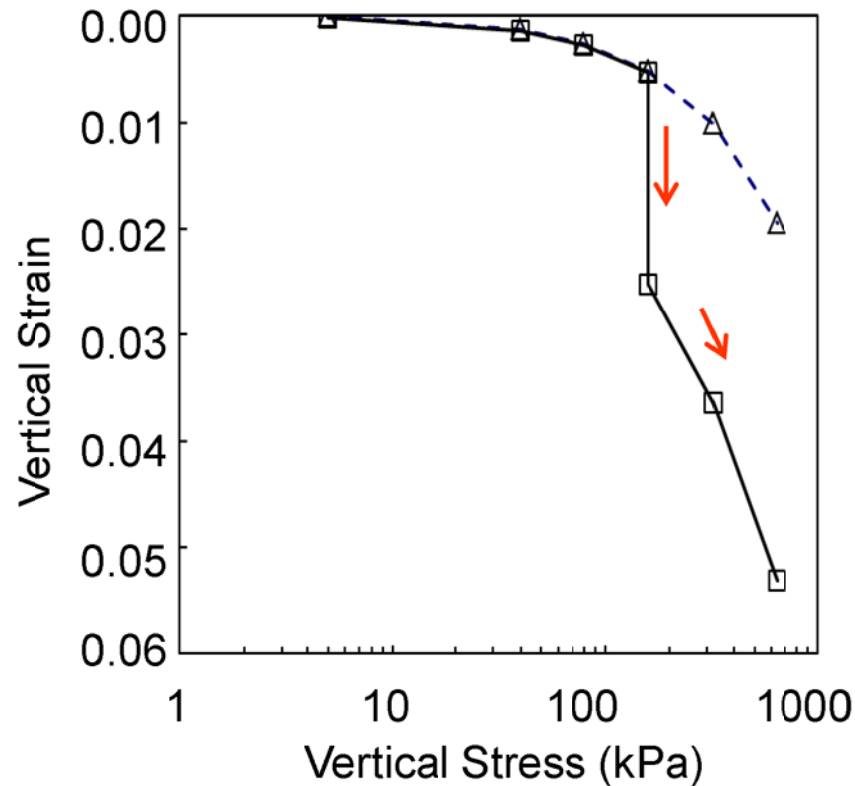
- DEM (PFC2D) used to modeling soluble mixtures in K_0 loading condition



- $d_{\text{sand}} = 0.36\text{mm}$, $d_{\text{salt}} = 0.25\text{mm}$
- $k_n = 10^8 \text{ N/m}$, $k_s = 5 \times 10^7 \text{ N/m}$
- $\rho = 2650\text{kg/m}^3$
- $\text{sf} = 10\%$
- Simulation: created walls, generated particles, equilibrium state, consolidated to desired stress level: 160kPa
- Dissolved particles by slowly reducing radii of soluble particles : 0.9999

Stress – strain – Numerical simulation

■ Stress – Strain

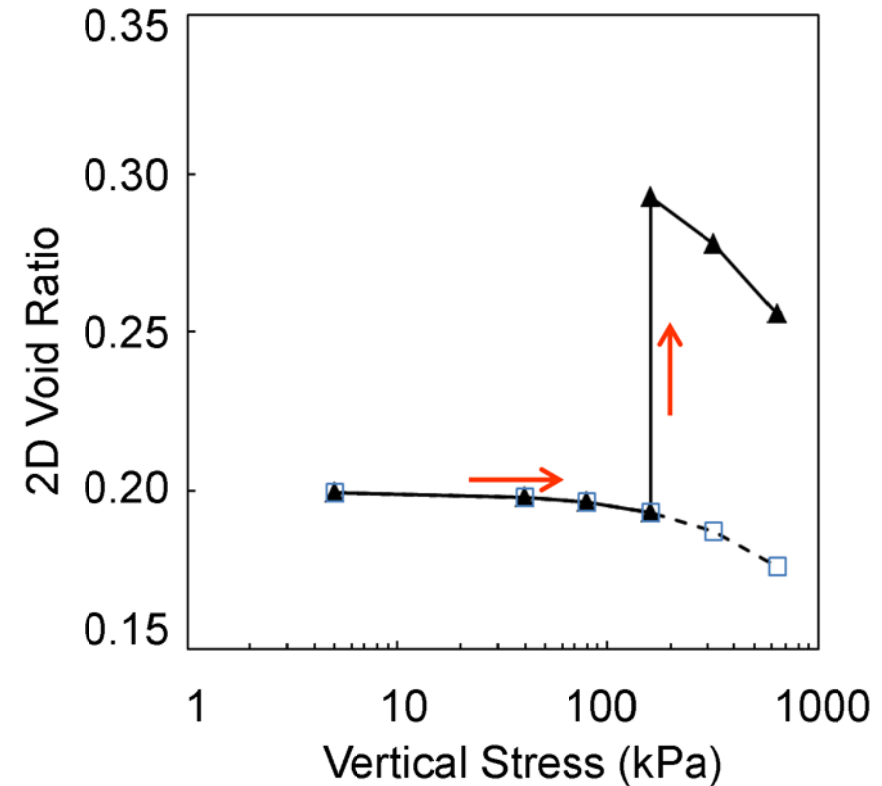


■ After saturation:

■ $\epsilon_v \uparrow$

∴ Total volume ↓ after dissolution

■ Stress – Void ratio



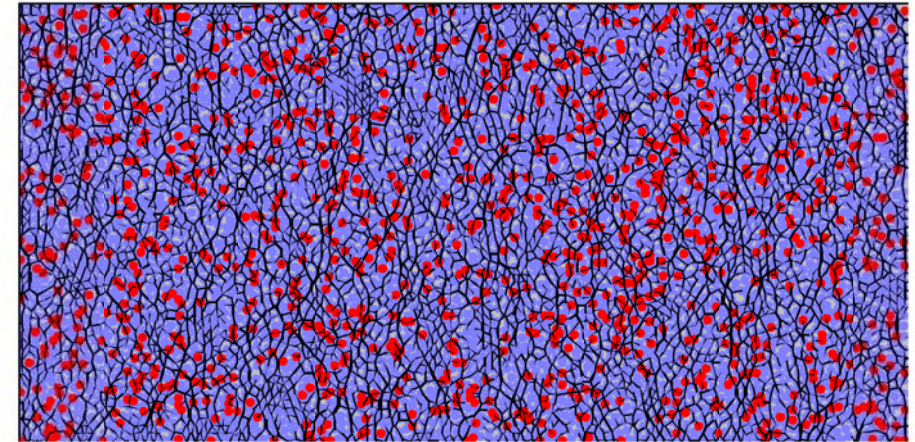
■ After saturation:

■ $e_{2D} \uparrow\uparrow$

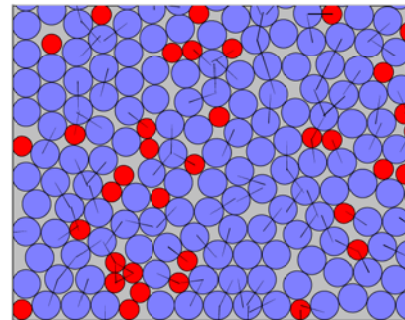
∴ Specimen getting loosen

Discussion – Fabric, force chain

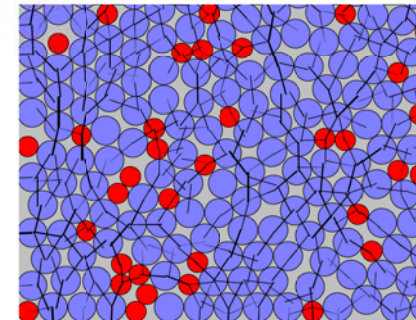
- No dissolution



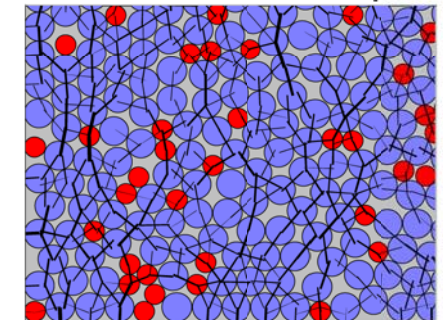
160Kpa



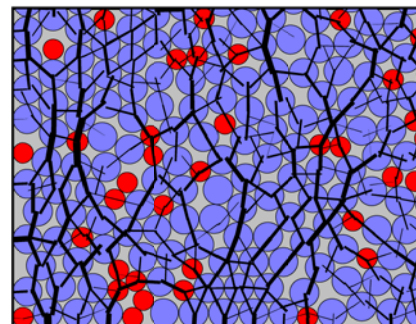
5Kpa



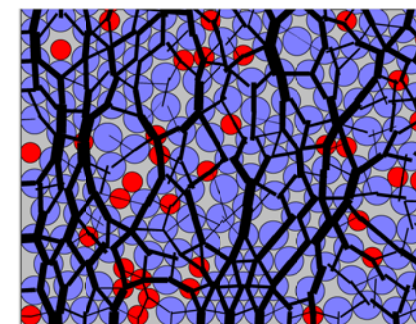
40Kpa



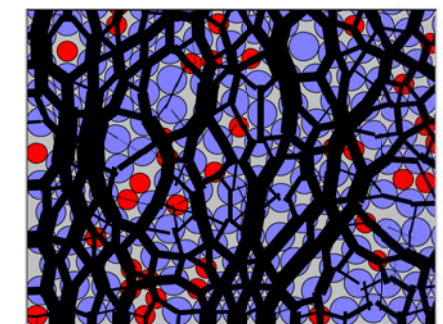
80Kpa



160Kpa



320Kpa

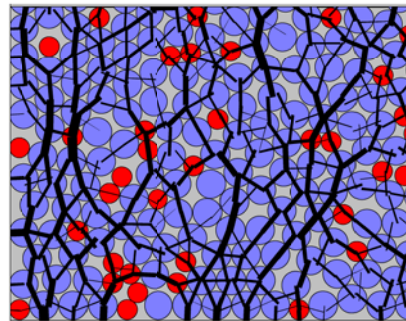
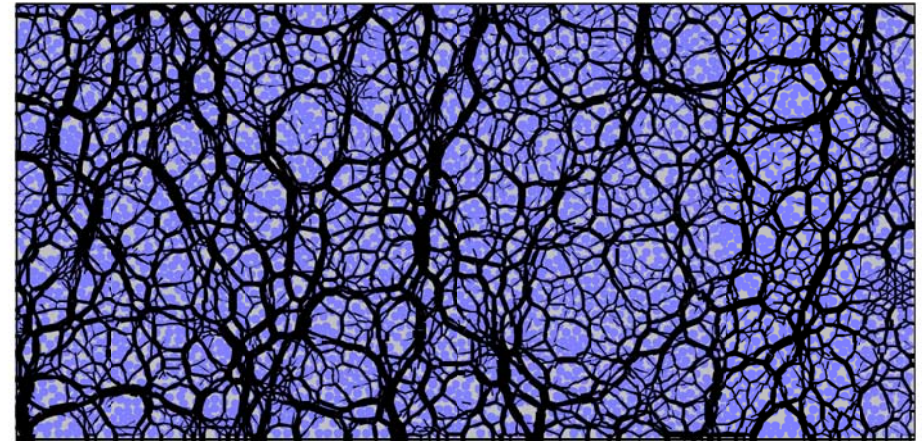


640Kpa

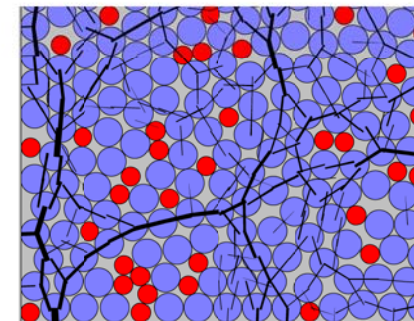
Discussion – Fabric, force chain

- Dissolution

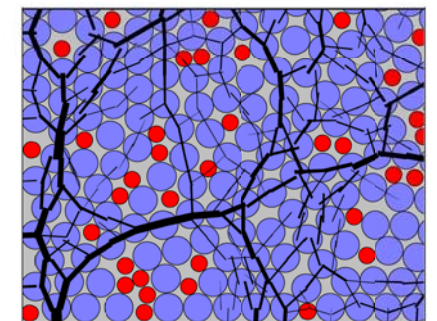
160Kpa



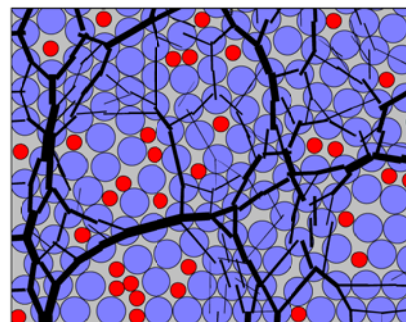
$R/R_0 = 1.0$



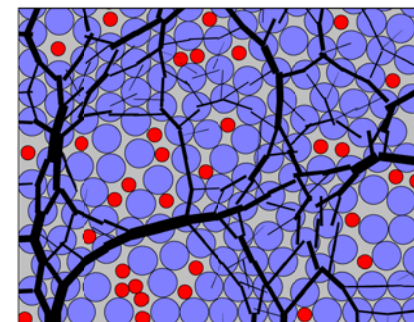
$R/R_0 = 0.9$



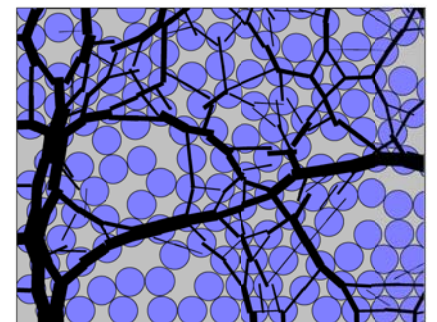
$R/R_0 = 0.82$



$R/R_0 = 0.74$



$R/R_0 = 0.67$

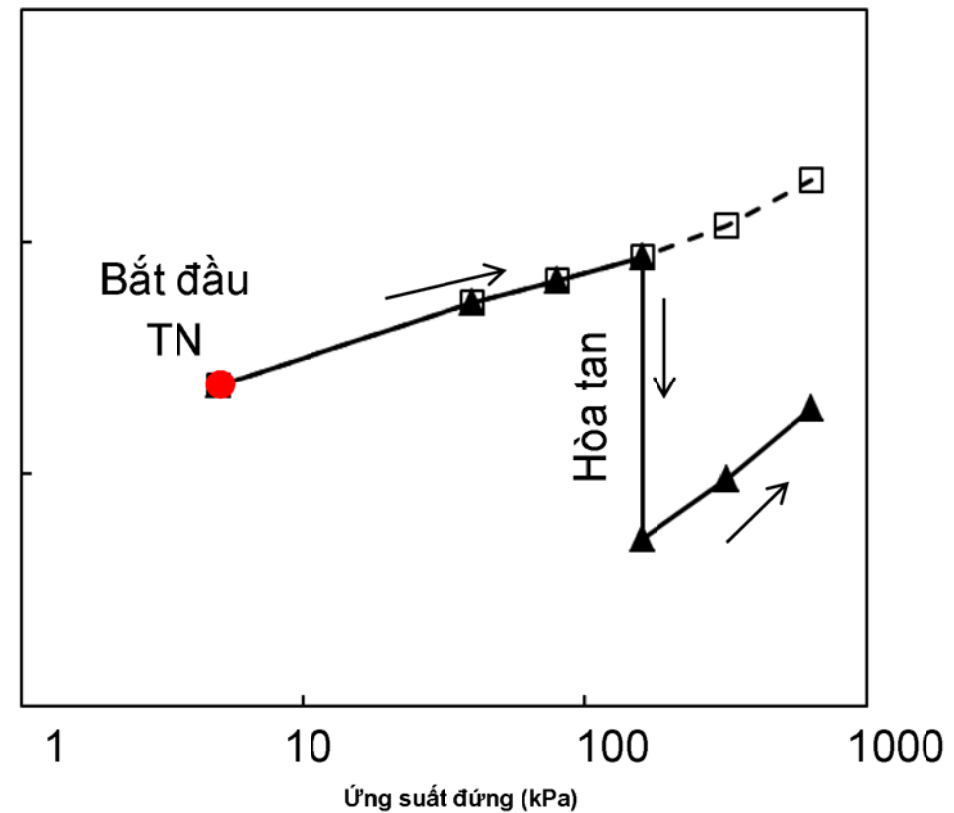


$R/R_0 = 0.0$

Discussion – Coordination number

- Coordination Number

$$C = \frac{2M_{pp} + M_{pw}}{N}$$



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Summary - stiffness characteristics

- Artificial specimens : sand-salt with various salt fraction
- Experiments in conventional oedometer cell + BE
- After dissolution,
 - Vertical strain increases
 - Void ratio increases
 - Shear wave velocity decreases
- The changes is proportional with initial salt fraction
- Dissolution → increase of void ratio and reduce particle contact
- DEM simulations :
 - same trend as experiments
 - show inside process of the soluble mixtures